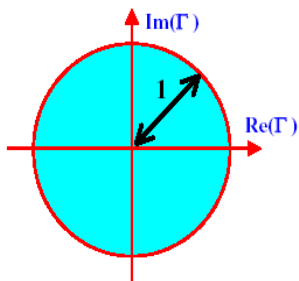


## The Smith Chart

- The Smith Chart is simply a graphical calculator for computing impedance as a function of reflection coefficient.
- Many problems can be easily visualized with the Smith Chart
- The Smith chart is one of the most useful graphical tools for high frequency circuit applications. The chart provides a clever way to visualize complex functions.

From a mathematical point of view, the Smith chart is simply a representation of all possible complex impedances with respect to coordinates defined by the reflection coefficient.



The domain of definition of the reflection coefficient is a circle of radius 1 in the complex plane. This is also the domain of the Smith chart.

The goal of the Smith chart is to identify **all possible impedances** on the domain of existence of the reflection coefficient. To do so, we start from the general definition of **line impedance** (which is equally applicable to the load impedance)

$$Z(d) = \frac{V(d)}{I(d)} = Z_0 \frac{1 + \Gamma(d)}{1 - \Gamma(d)}$$

This provides the complex function  $Z(d) = f\{\text{Re}(\Gamma), \text{Im}(\Gamma)\}$  that we want to graph. It is obvious that the result would be applicable only to lines with exactly characteristic impedance  $Z_0$ .

In order to obtain **universal** curves, we introduce the concept of **normalized impedance**

$$z(d) = \frac{Z(d)}{Z_0} = \frac{1 + \Gamma(d)}{1 - \Gamma(d)}$$

The **normalized impedance** is represented on the **Smith chart** by using families of curves that identify the **normalized resistance**  $r$  (real part) and the **normalized reactance**  $x$  (imaginary part)

$$z(d) = \text{Re}(z) + j \text{Im}(z) = r + jx$$

Let's represent the **reflection coefficient** in terms of its coordinates

$$\Gamma(d) = \text{Re}(\Gamma) + j \text{Im}(\Gamma)$$

Now we can write

$$\begin{aligned} r + jx &= \frac{1 + \text{Re}(\Gamma) + j \text{Im}(\Gamma)}{1 - \text{Re}(\Gamma) - j \text{Im}(\Gamma)} \\ &= \frac{1 - \text{Re}^2(\Gamma) - \text{Im}^2(\Gamma) + j2 \text{Im}(\Gamma)}{(1 - \text{Re}(\Gamma))^2 + \text{Im}^2(\Gamma)} \end{aligned}$$

The **real part** gives

$$r = \frac{1 - \operatorname{Re}^2(\Gamma) - \operatorname{Im}^2(\Gamma)}{(1 - \operatorname{Re}(\Gamma))^2 + \operatorname{Im}^2(\Gamma)}$$

Add a quantity equal to zero

$$r(\operatorname{Re}(\Gamma) - 1)^2 + (\operatorname{Re}^2(\Gamma) - 1) + r\operatorname{Im}^2(\Gamma) + \operatorname{Im}^2(\Gamma) + \frac{1}{1+r} - \frac{1}{1+r} = 0$$

$$\left[ r(\operatorname{Re}(\Gamma) - 1)^2 + (\operatorname{Re}^2(\Gamma) - 1) + \frac{1}{1+r} \right] + (1+r)\operatorname{Im}^2(\Gamma) = \frac{1}{1+r}$$

$$(1+r) \left[ \operatorname{Re}^2(\Gamma) - 2\operatorname{Re}(\Gamma)\frac{r}{1+r} + \frac{r^2}{(1+r)^2} \right] + (1+r)\operatorname{Im}^2(\Gamma) = \frac{1}{1+r}$$

$$\Rightarrow \left[ \operatorname{Re}(\Gamma) - \frac{r}{1+r} \right]^2 + \operatorname{Im}^2(\Gamma) = \left( \frac{1}{1+r} \right)^2$$

Equation of a circle

The **imaginary part** gives

$$x = \frac{2\operatorname{Im}(\Gamma)}{(1 - \operatorname{Re}(\Gamma))^2 + \operatorname{Im}^2(\Gamma)}$$

Multiply by  $x$  and add a quantity equal to zero

$$x^2 \left[ (1 - \operatorname{Re}(\Gamma))^2 + \operatorname{Im}^2(\Gamma) \right] - 2x\operatorname{Im}(\Gamma) + 1 - 1 = 0$$

$$\left[ (1 - \operatorname{Re}(\Gamma))^2 + \operatorname{Im}^2(\Gamma) \right] - \frac{2}{x}\operatorname{Im}(\Gamma) + \frac{1}{x^2} = \frac{1}{x^2}$$

$$(1 - \operatorname{Re}(\Gamma))^2 + \left[ \operatorname{Im}^2(\Gamma) - \frac{2}{x}\operatorname{Im}(\Gamma) + \frac{1}{x^2} \right] = \frac{1}{x^2}$$

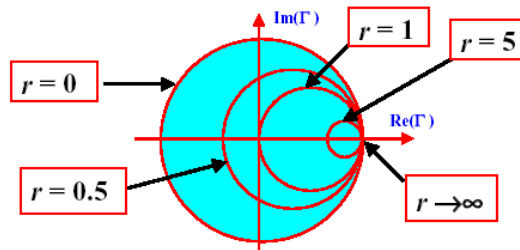
$$\Rightarrow (\operatorname{Re}(\Gamma) - 1)^2 + \left[ \operatorname{Im}(\Gamma) - \frac{1}{x} \right]^2 = \frac{1}{x^2}$$

Equation of a circle

The result for the **real part** indicates that on the complex plane with coordinates  $(\text{Re}(\Gamma), \text{Im}(\Gamma))$  all the possible impedances with a given normalized resistance  $r$  are found on a **circle** with

$$\text{Center} = \left\{ \frac{r}{1+r}, 0 \right\} \quad \text{Radius} = \frac{1}{1+r}$$

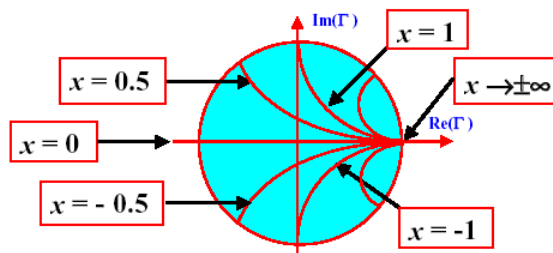
As the normalized resistance  $r$  varies from  $0$  to  $\infty$ , we obtain a family of circles completely contained inside the domain of the reflection coefficient  $|\Gamma| \leq 1$ .

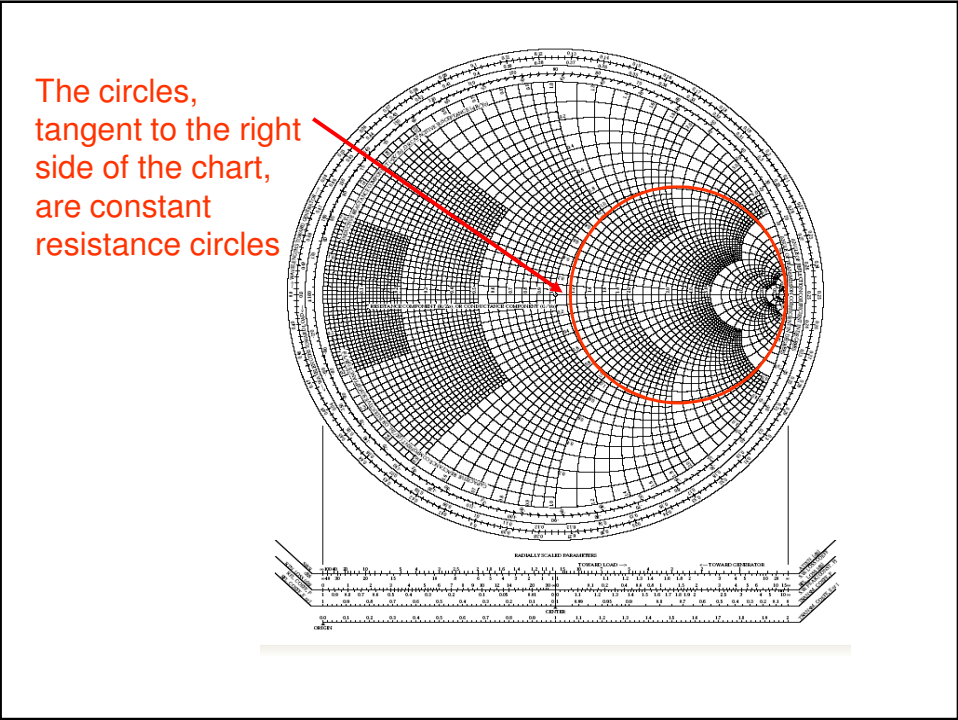
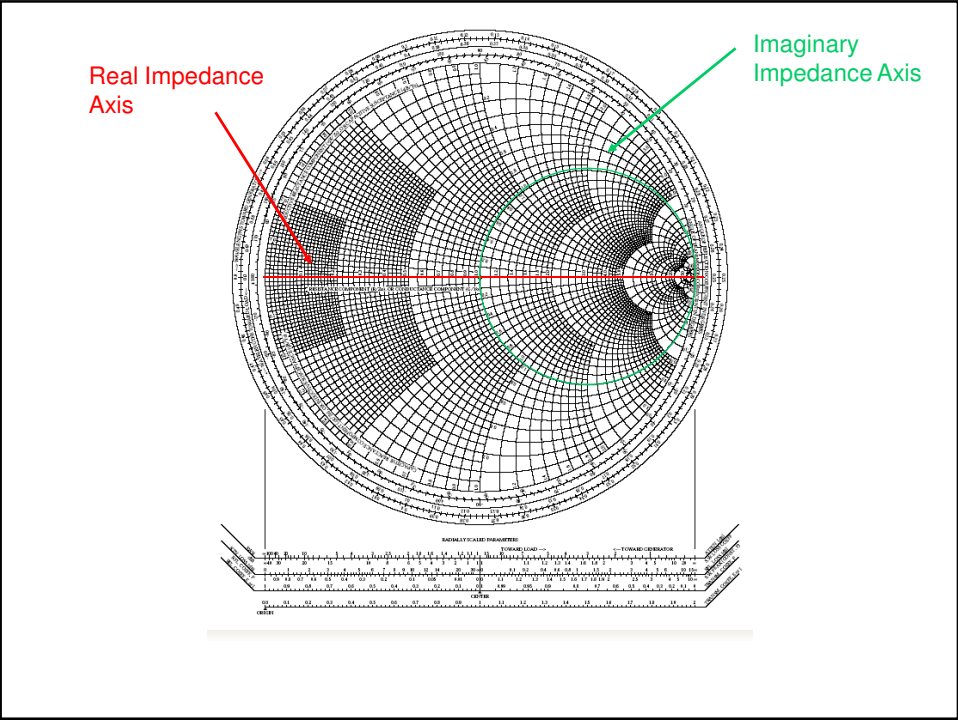


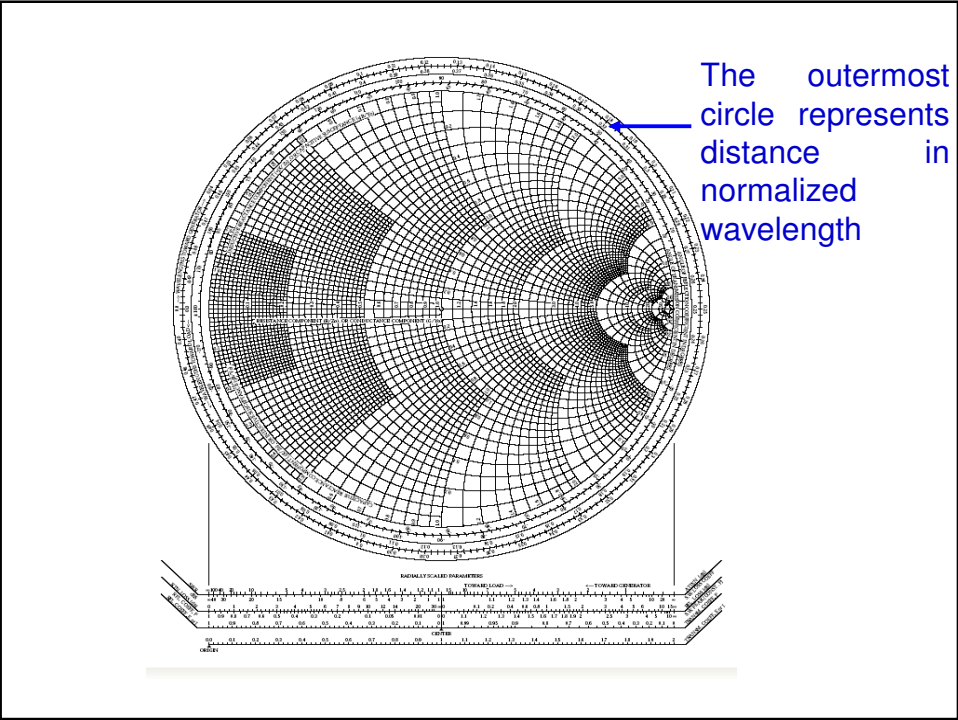
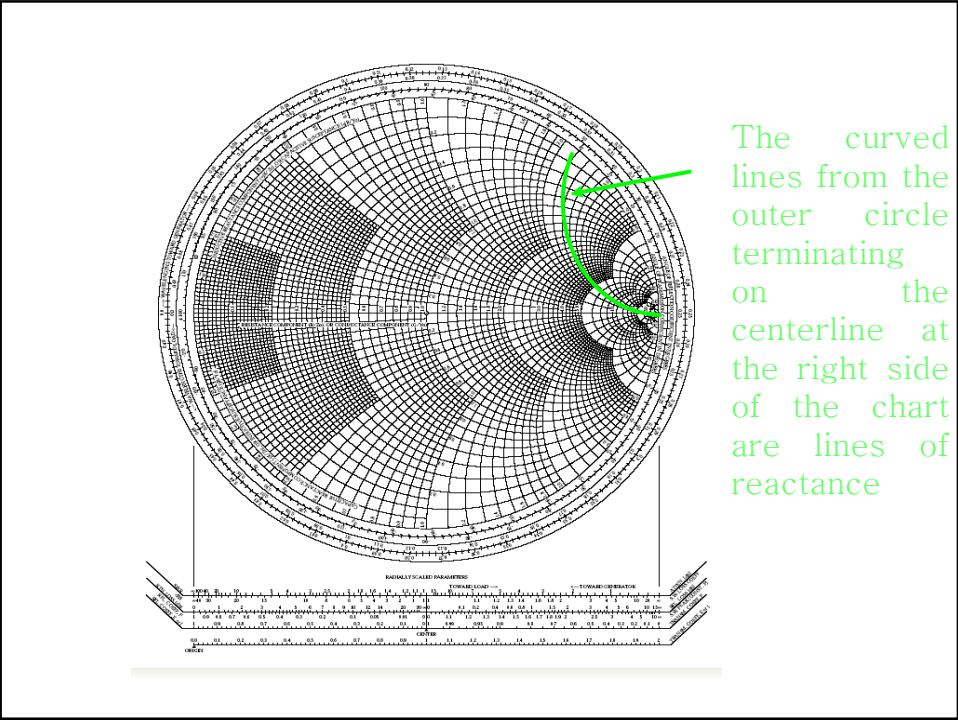
The result for the **imaginary part** indicates that on the complex plane with coordinates  $(\text{Re}(\Gamma), \text{Im}(\Gamma))$  all the possible impedances with a given normalized reactance  $x$  are found on a **circle** with

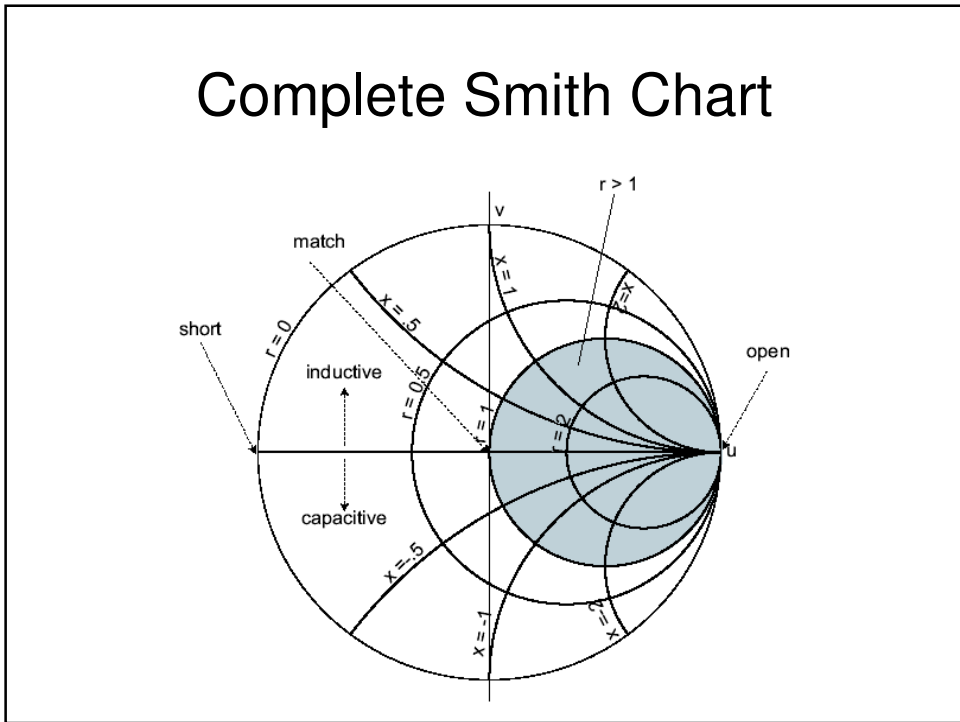
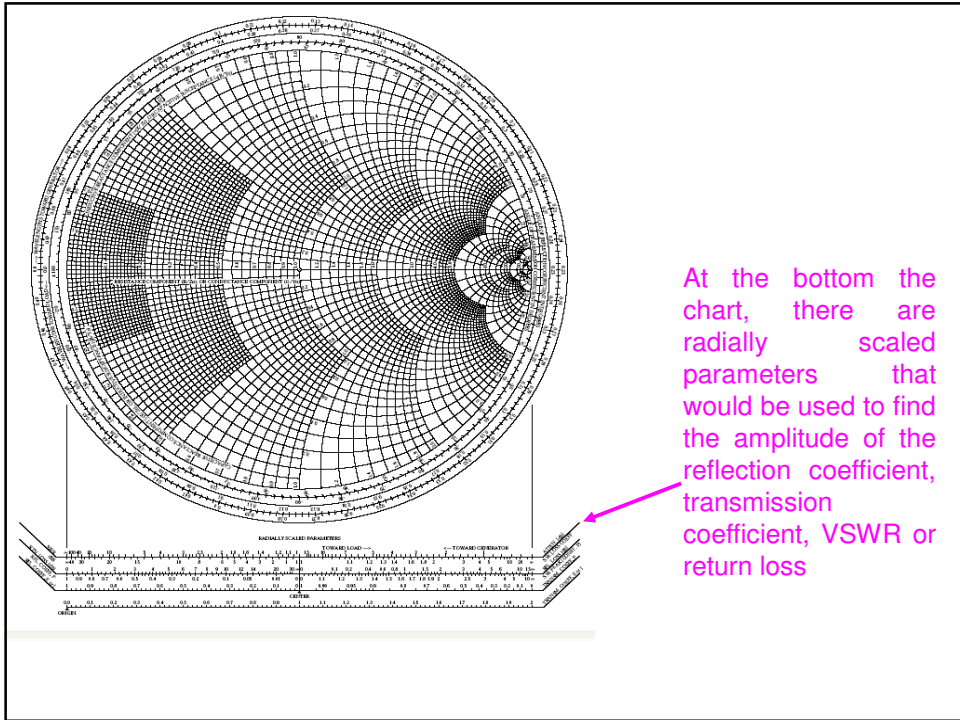
$$\text{Center} = \left\{ 1, \frac{1}{x} \right\} \quad \text{Radius} = \frac{1}{x}$$

As the normalized reactance  $x$  varies from  $-\infty$  to  $\infty$ , we obtain a family of arcs contained inside the domain of the reflection coefficient  $|\Gamma| \leq 1$ .

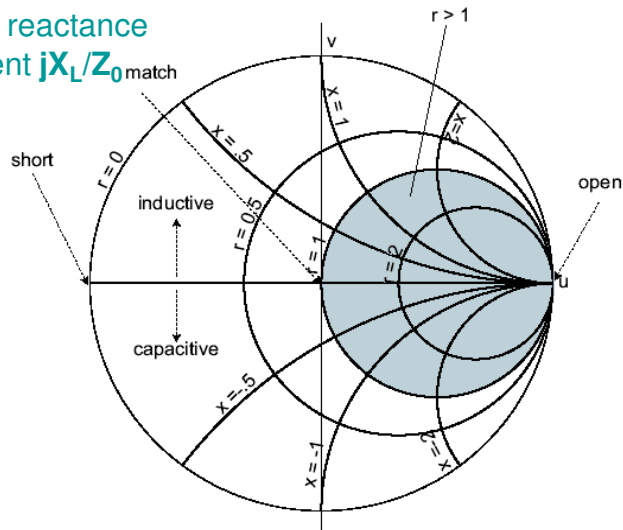




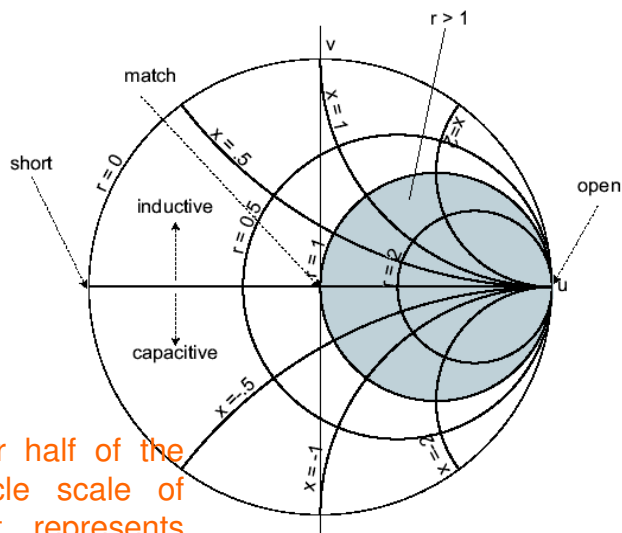




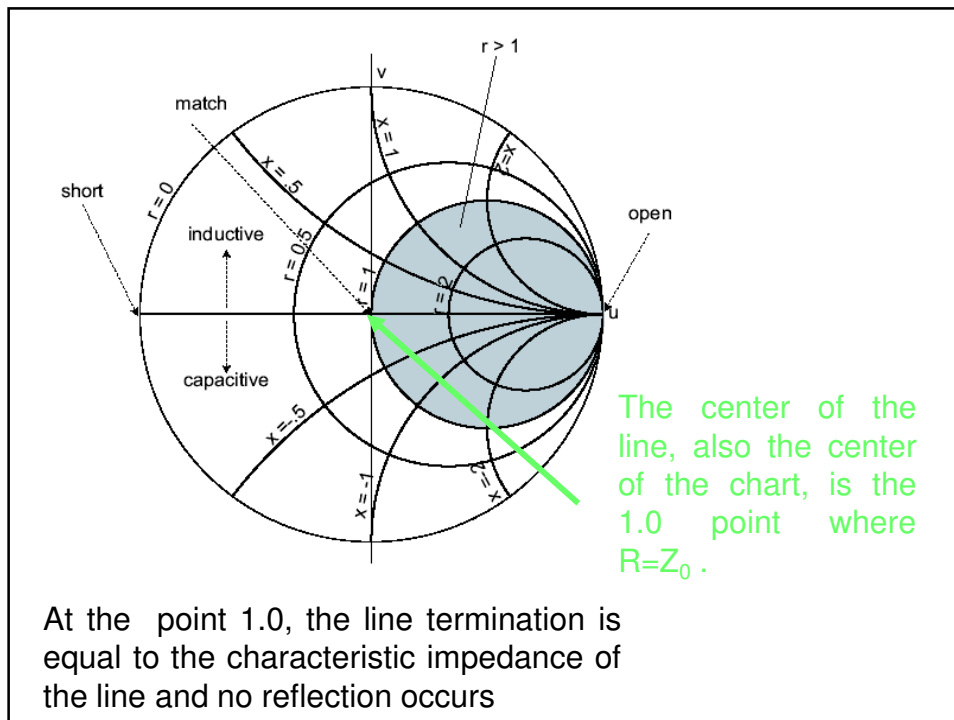
The upper half of the outer circle scale of the chart represents the inductive reactance component  $jX_L/Z_{0\text{match}}$



The lower half of the outer circle scale of the chart represents the capacitive reactance component  $-jX_c/Z_0$







## Smith Chart

- The outside of the chart shows location on the line in wavelengths.
- The combination of intersecting circles inside the chart allow us to locate the normalized impedance and then to find the impedance anywhere on the line.
- All impedance values are normalized with respect to the characteristic impedance of the transmission line.

- One revolution of the chart on the outermost circle is one-half wavelength.
- Impedances, voltages, currents, etc. all repeat every half wavelength
- The magnitude of the reflection coefficient, the standing wave ratio (SWR) do not change, so they characterize the voltage & current patterns on the line

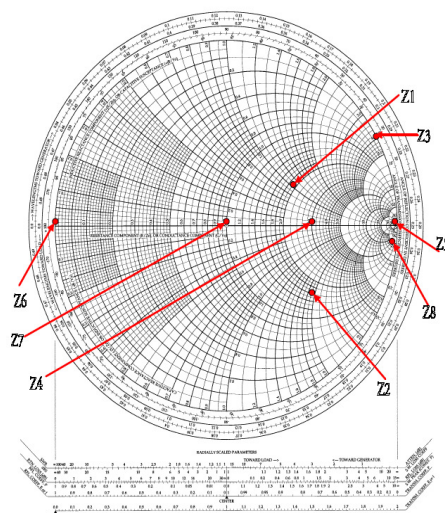
## Smith Chart

- Impedance divided by line impedance (50 Ohms)

- $Z_1 = 100 + j50$
- $Z_2 = 75 - j100$
- $Z_3 = j200$
- $Z_4 = 150$
- $Z_5 = \text{infinity}$  (an open circuit)
- $Z_6 = 0$  (a short circuit)
- $Z_7 = 50$
- $Z_8 = 184 - j900$

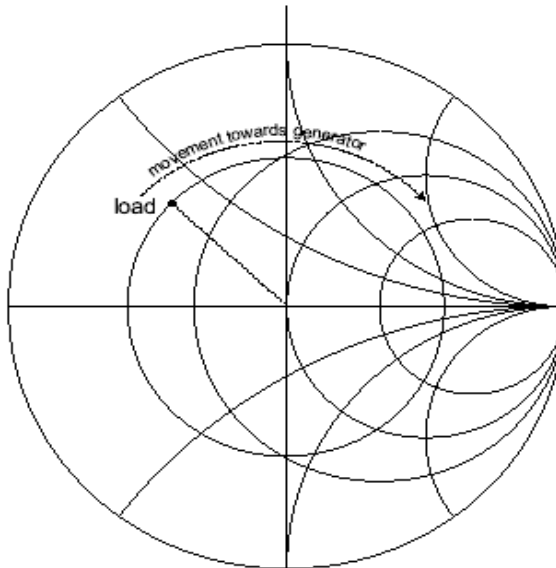
- Then, normalize and plot. The points are plotted as follows:

- $z_1 = 2 + j$
- $z_2 = 1.5 - j2$
- $z_3 = j4$
- $z_4 = 3$
- $z_5 = \text{infinity}$
- $z_6 = 0$
- $z_7 = 1$
- $z_8 = 3.68 - j18$



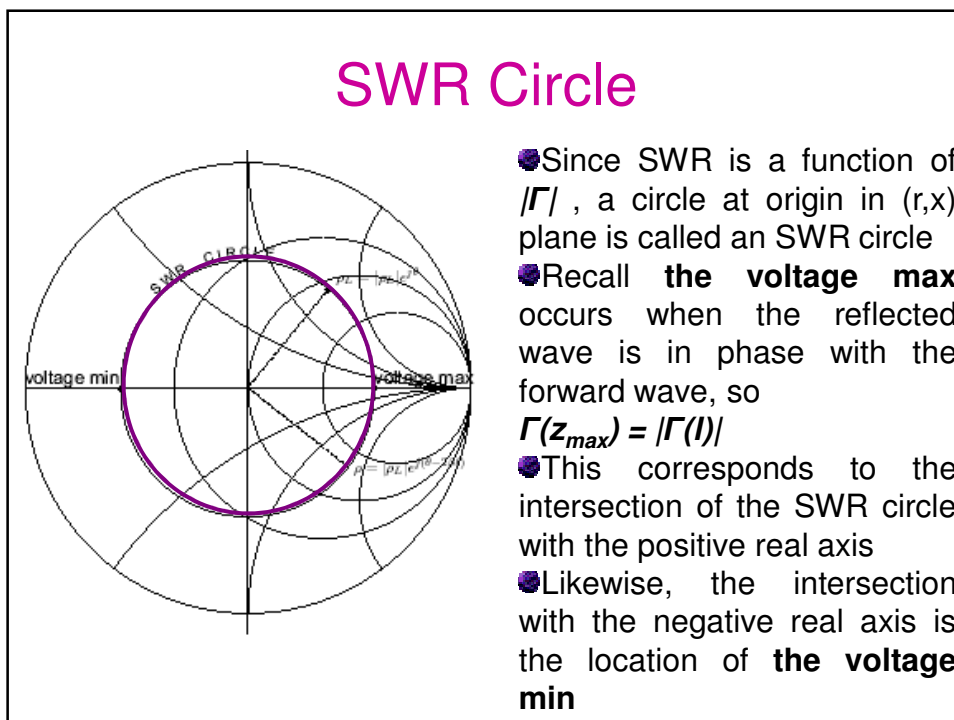
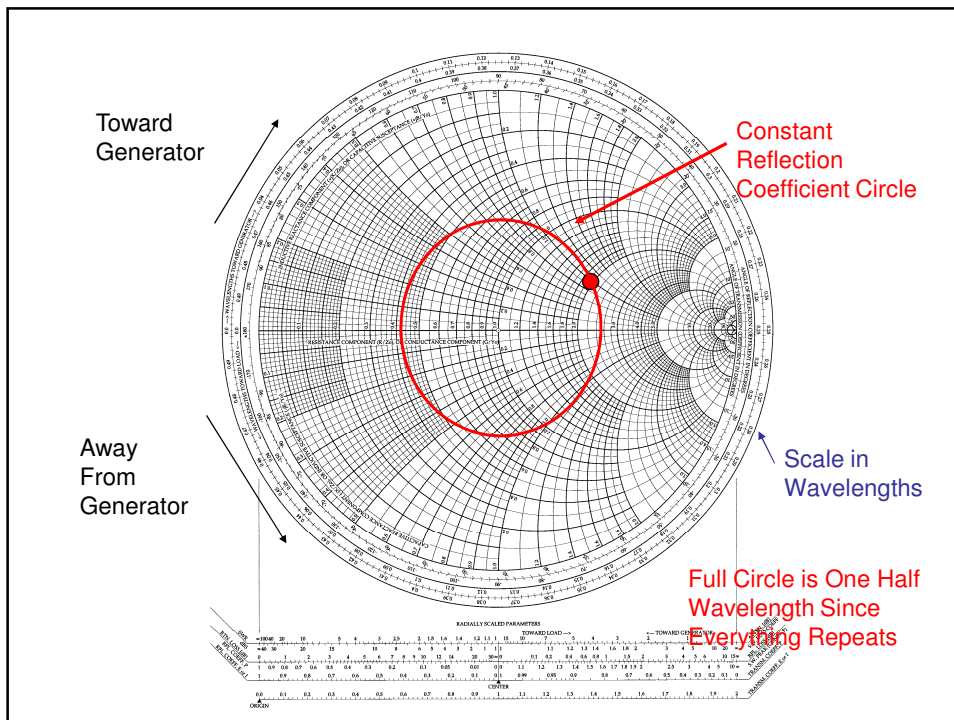
## Motion Towards Generator

- Moving towards generator means  $\Gamma(-l) = |\Gamma| e^{-j\beta l}$ , or clockwise motion.
- We're back to where we started when  $2\beta l = 2\pi$ , or  $l = \lambda/2$ .
- Thus the impedance is periodic.



## Smith Chart

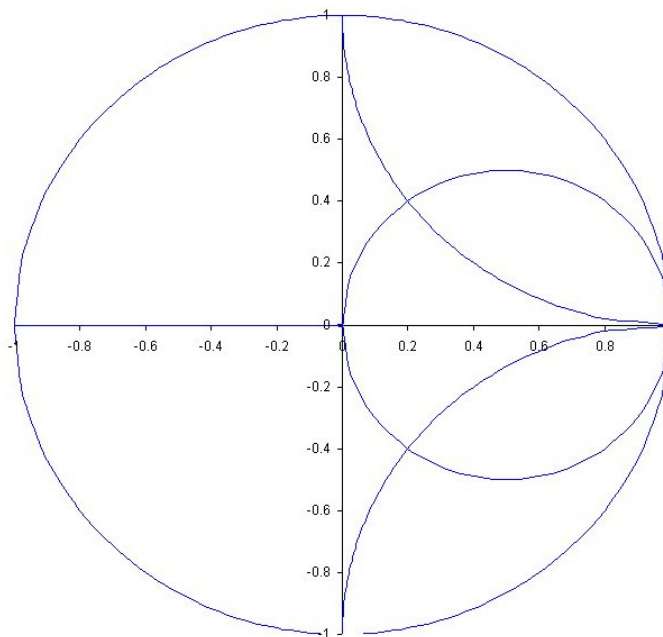
- Thus, the first step in analyzing a transmission line is to locate the normalized load impedance on the chart
- Next, a circle is drawn that represents the reflection coefficient or SWR. The center of the circle is the center of the chart. The circle passes through the normalized load impedance
- Any point on the line is found on this circle. Rotate clockwise to move toward the generator (away from the load)
- The distance moved on the line is indicated on the outside of the chart in wavelengths



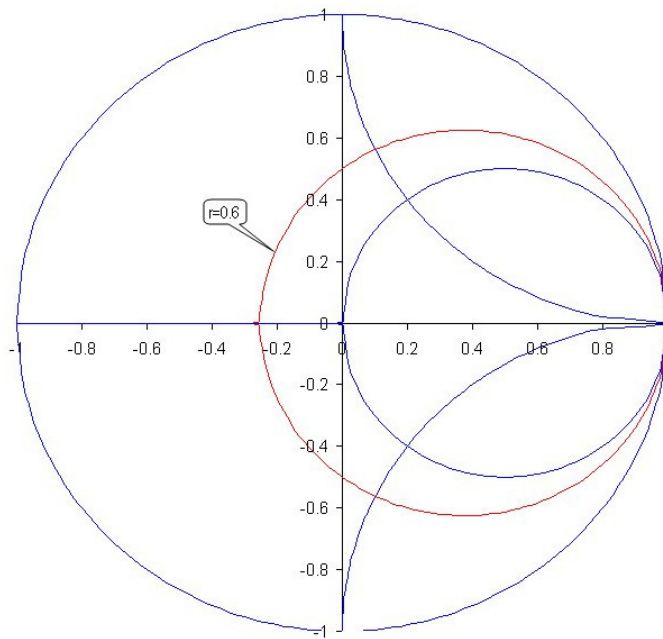
## Smith Chart Example

- First, locate the normalized impedance on the chart for  $Z_L = 30 + j70$  ( $Z_0=50$  ohm)
- Then draw the circle through the point
- The circle gives us the reflection coefficient (the radius of the circle) which can be read from the scale at the bottom of most charts
- Also note that exactly opposite to the normalized load is its admittance. Thus, the chart can also be used to find the admittance. We use this fact in stub matching

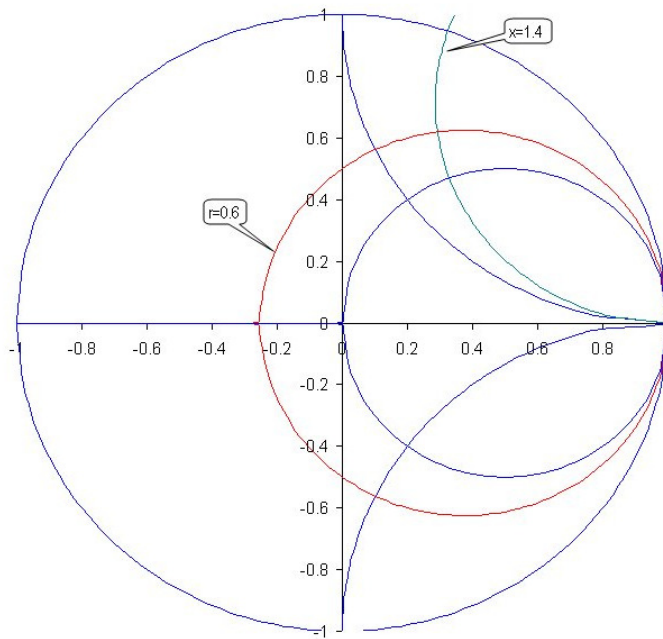
Start with the Smith Chart



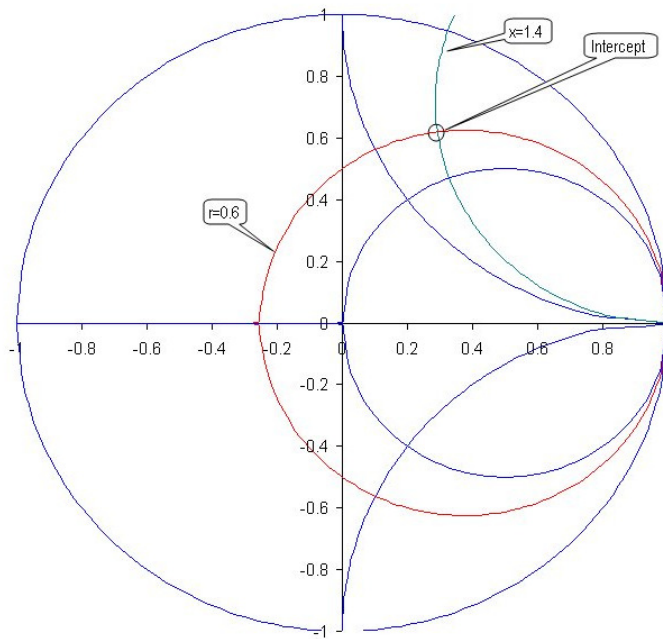
Locate r Circle of the normalized Load Impedance = Real part of ( $Z_L/Z_0$ )



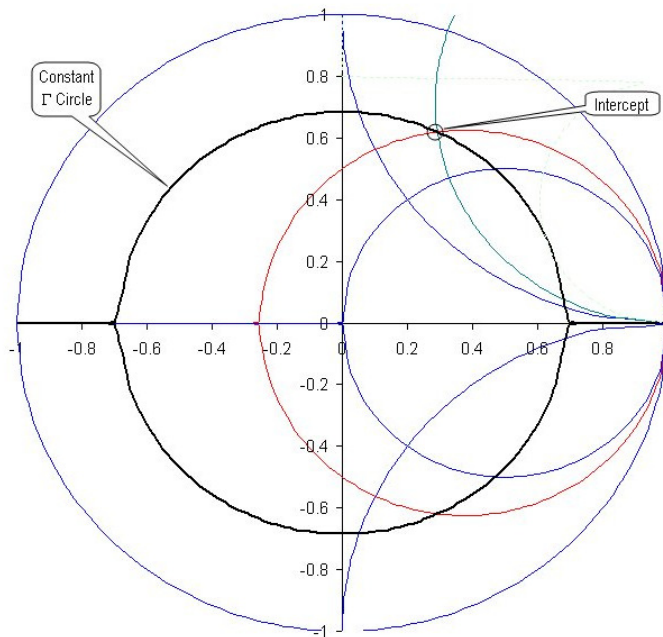
Locate the x Circle of the normalized Load Impedance = Imag part of ( $Z_L/Z_0$ )

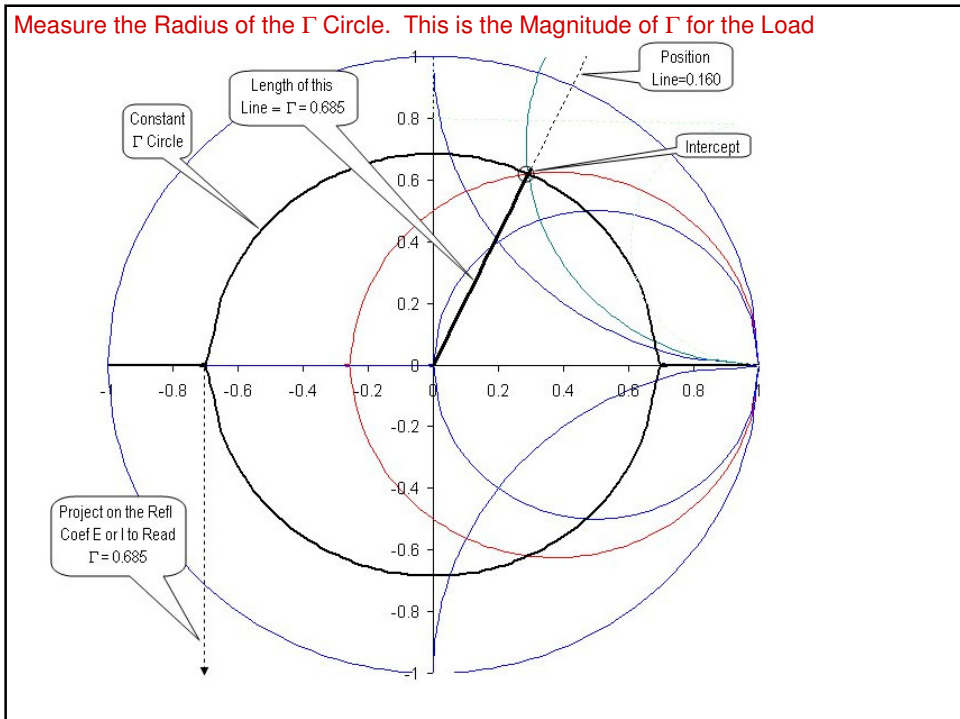
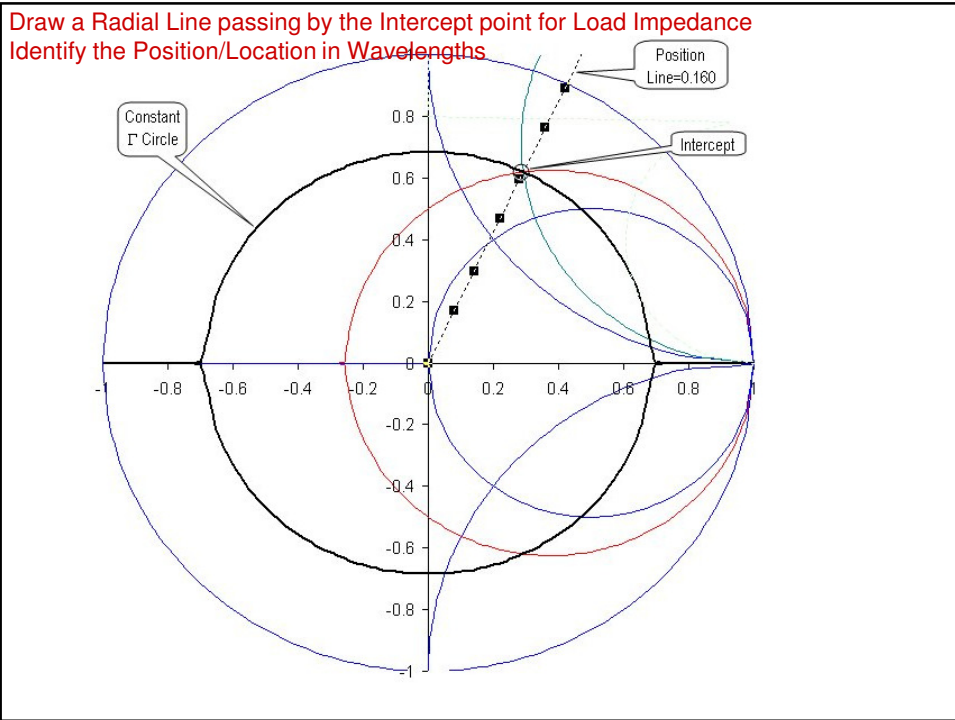


Locate the Intercept point of the  $r$  Circle and the  $x$  Circle for Load Impedance



Draw a constant  $\Gamma$  Circle passing by the Intercept point for Load Impedance







**Basic Smith Chart techniques for loss-less transmission lines**

- Given  $Z(d) \Rightarrow$  Find  $\Gamma(d)$   
Given  $\Gamma(d) \Rightarrow$  Find  $Z(d)$
- Given  $\Gamma_R$  and  $Z_R \Rightarrow$  Find  $\Gamma(d)$  and  $Z(d)$   
Given  $\Gamma(d)$  and  $Z(d) \Rightarrow$  Find  $\Gamma_R$  and  $Z_R$
- Find  $d_{\max}$  and  $d_{\min}$  (maximum and minimum locations for the voltage standing wave pattern)
- Find the Voltage Standing Wave Ratio (VSWR)
- Given  $Z(d) \Rightarrow$  Find  $Y(d)$   
Given  $Y(d) \Rightarrow$  Find  $Z(d)$

**Given  $Z(d) \Rightarrow$  Find  $\Gamma(d)$** 

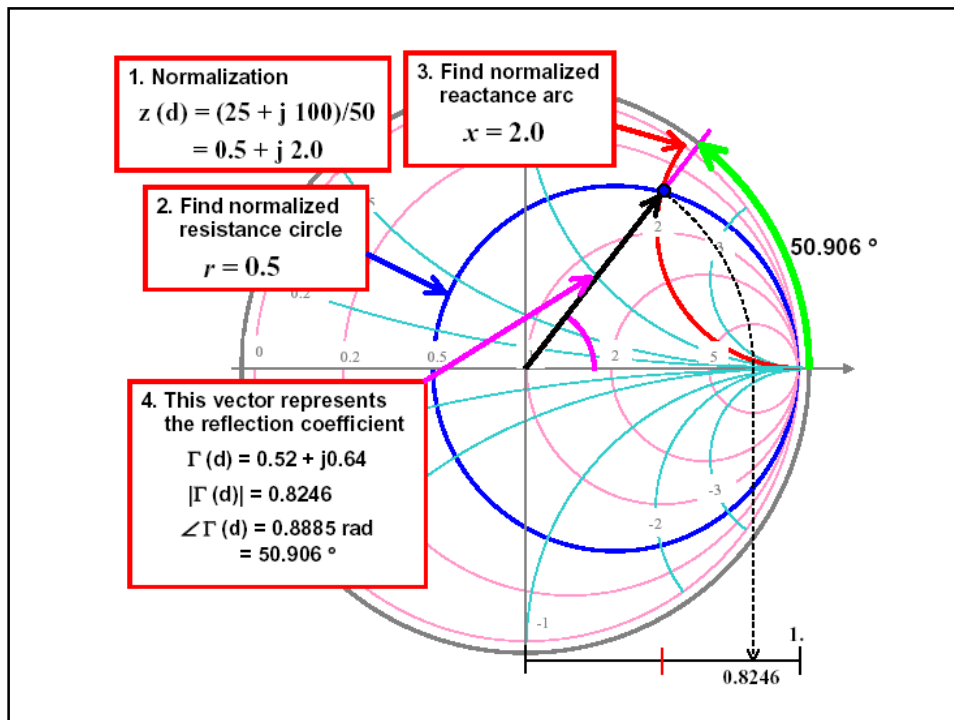
1. Normalize the impedance

$$z(d) = \frac{Z(d)}{Z_0} = \frac{R}{Z_0} + j \frac{X}{Z_0} = r + jx$$

2. Find the circle of constant normalized resistance  $r$
3. Find the arc of constant normalized reactance  $x$
4. The intersection of the two curves indicates the reflection coefficient in the complex plane. The chart provides directly the magnitude and the phase angle of  $\Gamma(d)$

**Example:** Find  $\Gamma(d)$ , given

$$Z(d) = 25 + j100 \Omega \quad \text{with} \quad Z_0 = 50 \Omega$$



Given  $\Gamma(d) \Rightarrow$  Find  $Z(d)$

1. Determine the complex point representing the given reflection coefficient  $\Gamma(d)$  on the chart.
2. Read the values of the normalized resistance  $r$  and of the normalized reactance  $x$  that correspond to the reflection coefficient point.
3. The normalized impedance is

$$z(d) = r + jx$$

and the actual impedance is

$$Z(d) = Z_0 z(d) = Z_0 (r + jx) = Z_0 r + j Z_0 x$$

Given  $\Gamma_R$  and  $Z_R \iff$  Find  $\Gamma(d)$  and  $Z(d)$

NOTE: the **magnitude** of the **reflection coefficient** is **constant** along a loss-less transmission line terminated by a specified load, since

$$|\Gamma(d)| = |\Gamma_R \exp(-j2\beta d)| = |\Gamma_R|$$

Therefore, on the complex plane, a **circle** with center at the **origin** and radius  $|\Gamma_R|$  represents all possible reflection coefficients found along the transmission line. When the **circle** of **constant magnitude** of the **reflection coefficient** is drawn on the Smith chart, one can determine the values of the line **impedance** at **any location**.

The graphical step-by-step procedure is:

1. Identify the load reflection coefficient  $\Gamma_R$  and the normalized load impedance  $Z_R$  on the Smith chart.

2. Draw the circle of constant reflection coefficient amplitude  $|\Gamma(d)| = |\Gamma_R|$ .
3. Starting from the point representing the load, travel on the circle in the **clockwise** direction, by an angle

$$\theta = 2\beta d = 2 \frac{2\pi}{\lambda} d$$

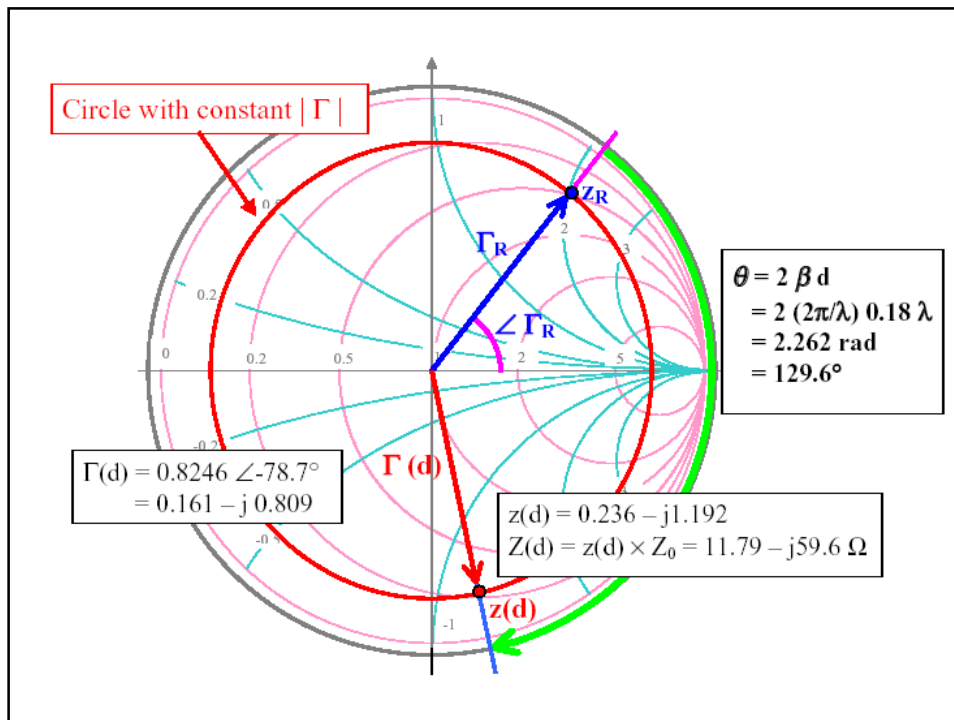
4. The new location on the chart corresponds to location **d** on the transmission line. Here, the values of  $\Gamma(d)$  and  $Z(d)$  can be read from the chart as before.

**Example:** Given

$$Z_R = 25 + j100 \Omega \quad \text{with} \quad Z_0 = 50 \Omega$$

find

$$Z(d) \quad \text{and} \quad \Gamma(d) \quad \text{for} \quad d = 0.18\lambda$$

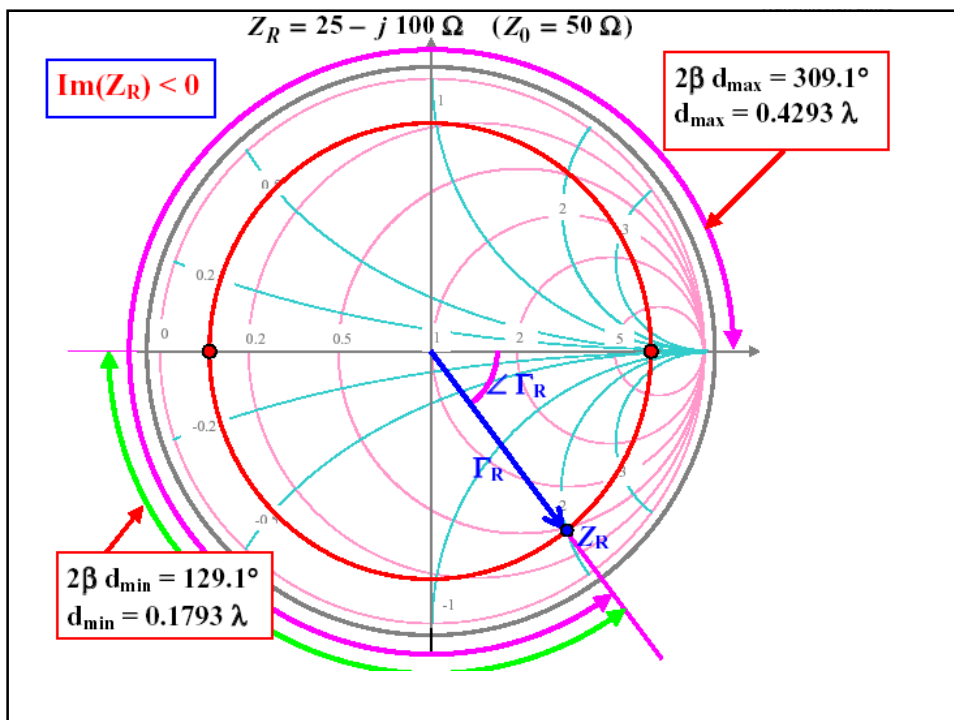
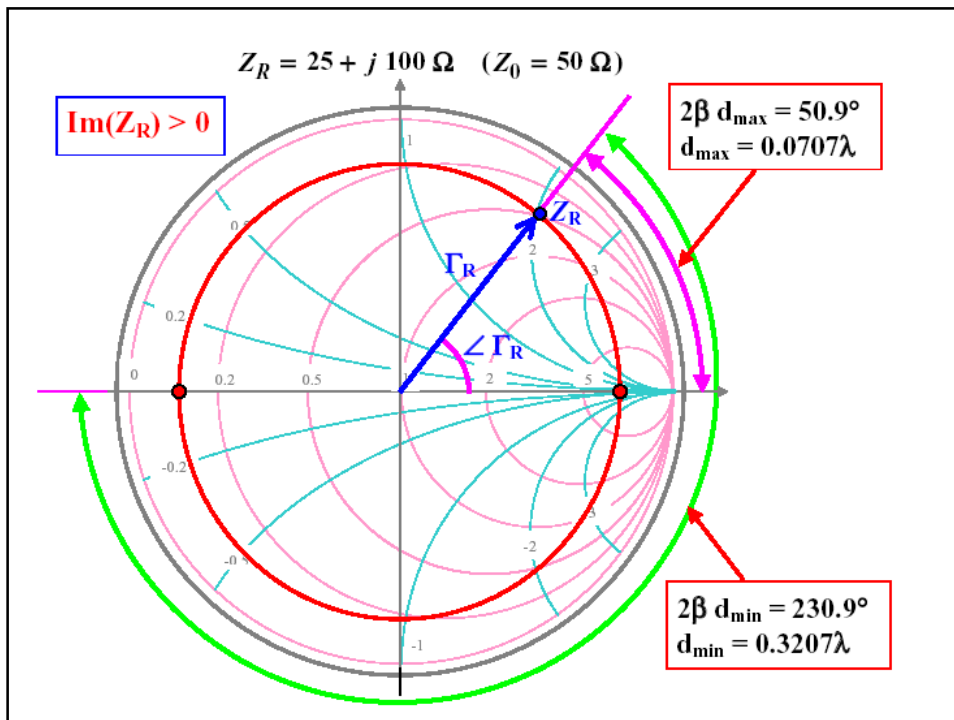


Given  $\Gamma_R$  and  $Z_R \Rightarrow$  Find  $d_{\max}$  and  $d_{\min}$

1. Identify on the Smith chart the load reflection coefficient  $\Gamma_R$  or the normalized load impedance  $Z_R$ .
2. Draw the circle of constant reflection coefficient amplitude  $|\Gamma(d)| = |\Gamma_R|$ . The circle intersects the real axis of the reflection coefficient at two points which identify  $d_{\max}$  (when  $\Gamma(d) = \text{Real positive}$ ) and  $d_{\min}$  (when  $\Gamma(d) = \text{Real negative}$ )
3. A commercial Smith chart provides an outer graduation where the distances normalized to the wavelength can be read directly. The angles, between the vector  $\Gamma_R$  and the real axis, also provide a way to compute  $d_{\max}$  and  $d_{\min}$ .

**Example:** Find  $d_{\max}$  and  $d_{\min}$  for

$$Z_R = 25 + j 100 \Omega ; Z_R = 25 - j 100 \Omega \quad (Z_0 = 50 \Omega)$$



Given  $\Gamma_R$  and  $Z_R \Rightarrow$  Find the Voltage Standing Wave Ratio (VSWR)

The Voltage standing Wave Ratio or **VSWR** is defined as

$$VSWR = \frac{V_{\max}}{V_{\min}} = \frac{1 + |\Gamma_R|}{1 - |\Gamma_R|}$$

The **normalized impedance** at a **maximum location** of the standing wave pattern is given by

$$z(d_{\max}) = \frac{1 + \Gamma(d_{\max})}{1 - \Gamma(d_{\max})} = \frac{1 + |\Gamma_R|}{1 - |\Gamma_R|} = VSWR!!!$$

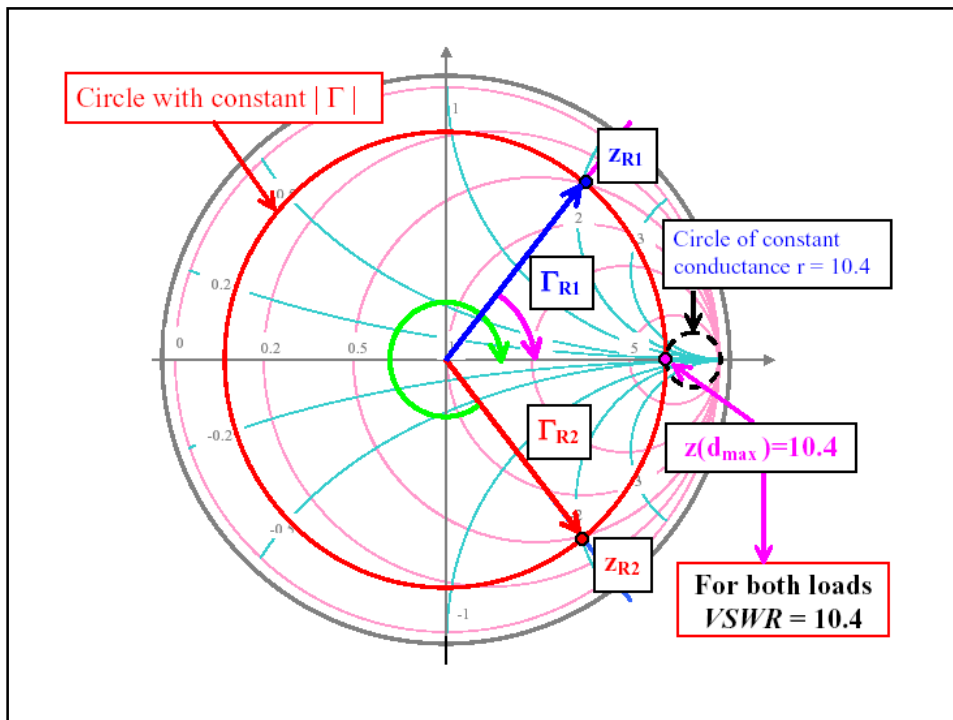
This quantity is always **real** and  $\geq 1$ . The VSWR is simply obtained on the Smith chart, by reading the value of the (real) normalized impedance, at the location  $d_{\max}$  where  $\Gamma$  is **real** and **positive**.

The graphical step-by-step procedure is:

1. Identify the load reflection coefficient  $\Gamma_R$  and the normalized load impedance  $Z_R$  on the Smith chart.
2. Draw the circle of constant reflection coefficient amplitude  $|\Gamma(d)| = |\Gamma_R|$ .
3. Find the intersection of this circle with the real positive axis for the reflection coefficient (corresponding to the transmission line location  $d_{\max}$ ).
4. A circle of **constant normalized resistance** will also intersect this point. Read or interpolate the value of the normalized resistance to determine the **VSWR**.

**Example:** Find the **VSWR** for

$$Z_{R1} = 25 + j100 \Omega ; Z_{R2} = 25 - j100 \Omega \quad (Z_0 = 50 \Omega)$$



Given  $Z(d) \iff$  Find  $Y(d)$

**Note:** The normalized impedance and admittance are defined as

$$z(d) = \frac{1 + \Gamma(d)}{1 - \Gamma(d)} \quad y(d) = \frac{1 - \Gamma(d)}{1 + \Gamma(d)}$$

Since

$$\Gamma\left(d + \frac{\lambda}{4}\right) = -\Gamma(d)$$

$$\Rightarrow z\left(d + \frac{\lambda}{4}\right) = \frac{1 + \Gamma\left(d + \frac{\lambda}{4}\right)}{1 - \Gamma\left(d + \frac{\lambda}{4}\right)} = \frac{1 - \Gamma(d)}{1 + \Gamma(d)} = y(d)$$

Keep in mind that the equality

$$z\left(d + \frac{\lambda}{4}\right) = y(d)$$

is only valid for **normalized** impedance and admittance. The **actual** values are given by

$$Z\left(d + \frac{\lambda}{4}\right) = Z_0 \cdot z\left(d + \frac{\lambda}{4}\right)$$

$$Y(d) = Y_0 \cdot y(d) = \frac{y(d)}{Z_0}$$

where  $Y_0 = 1/Z_0$  is the **characteristic admittance** of the transmission

line.

The graphical step-by-step procedure is:

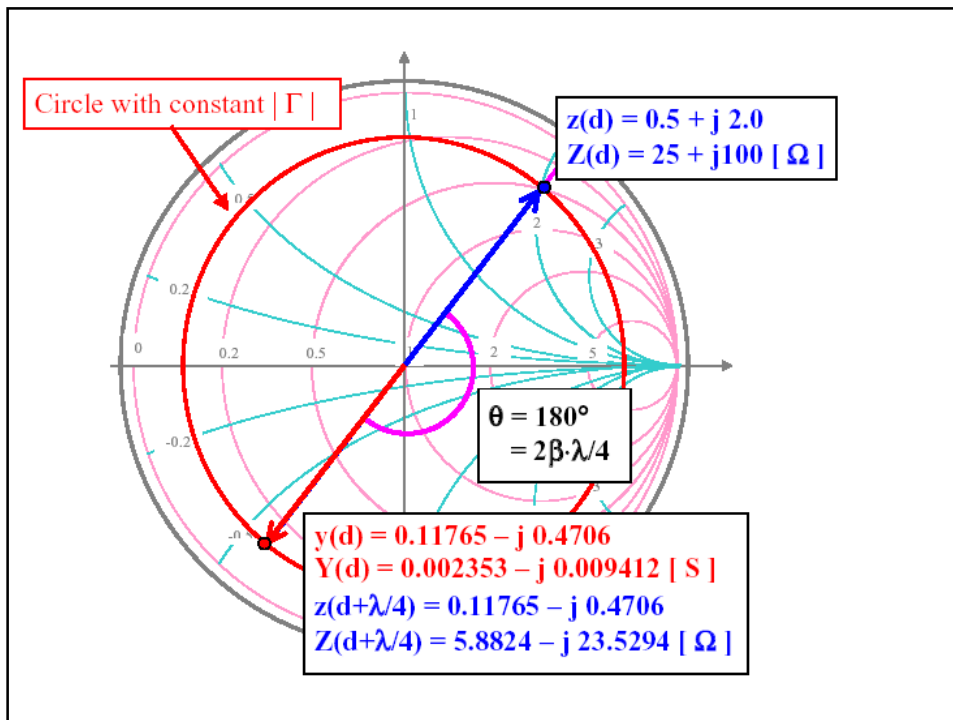
1. Identify the load reflection coefficient  $\Gamma_R$  and the normalized load impedance  $Z_R$  on the Smith chart.
2. Draw the circle of constant reflection coefficient amplitude  $|\Gamma(d)| = |\Gamma_R|$ .
3. The **normalized admittance** is located at a point on the circle of constant  $|\Gamma|$  which is diametrically opposite to the **normalized impedance**.

**Example:** Given

$$Z_R = 25 + j 100 \Omega \quad \text{with} \quad Z_0 = 50 \Omega$$

find  $Y_R$ .





The Smith chart can be used for line admittances, by shifting the space reference to the admittance location. After that, one can move on the chart just reading the numerical values as representing admittances.

Let's review the impedance-admittance terminology:

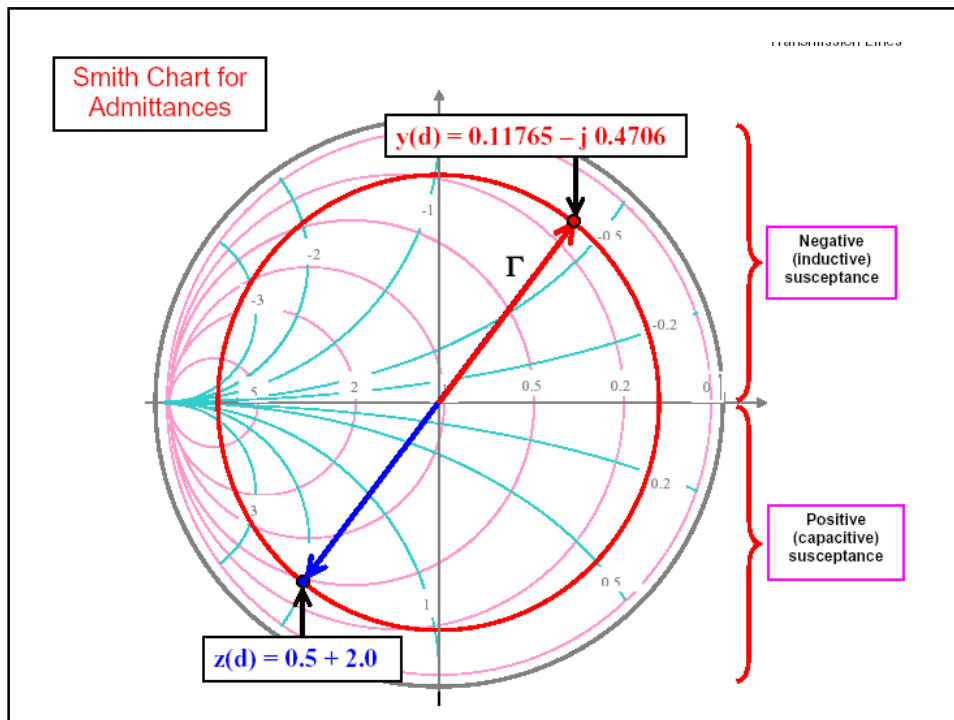
Impedance = Resistance + j Reactance

$$Z = R + jX$$

Admittance = Conductance + j Susceptance

$$Y = G + jB$$

On the impedance chart, the correct reflection coefficient is always represented by the vector corresponding to the normalized impedance. Charts specifically prepared for admittances are modified to give the correct reflection coefficient in correspondence of admittance.



Since related **impedance** and **admittance** are on opposite sides of the same Smith chart, the imaginary parts always have different sign.

Therefore, a **positive (inductive) reactance** corresponds to a **negative (inductive) susceptance**, while a **negative (capacitive) reactance** corresponds to a **positive (capacitive) susceptance**.

Numerically, we have

$$z = r + jx \quad y = g + jb = \frac{1}{r + jx}$$

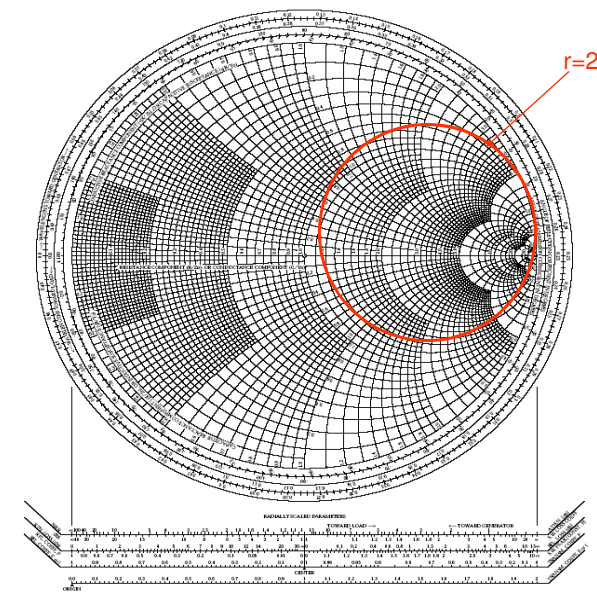
$$y = \frac{r - jx}{(r + jx)(r - jx)} = \frac{r - jx}{r^2 + x^2}$$

$$\Rightarrow \quad g = \frac{r}{r^2 + x^2} \quad b = -\frac{x}{r^2 + x^2}$$

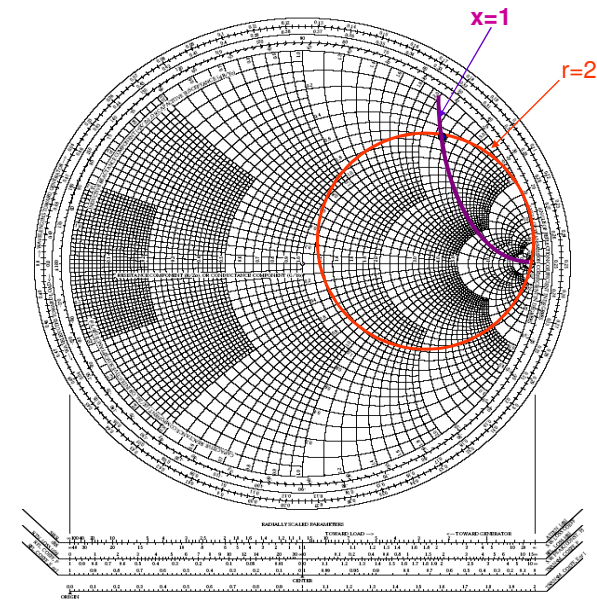
## Example: Smith Chart operation using admittances

- A load of  $Z_L=100+j50\Omega$  line. What are the load admittance and the input admittance if the line is  $0.15\lambda$  long

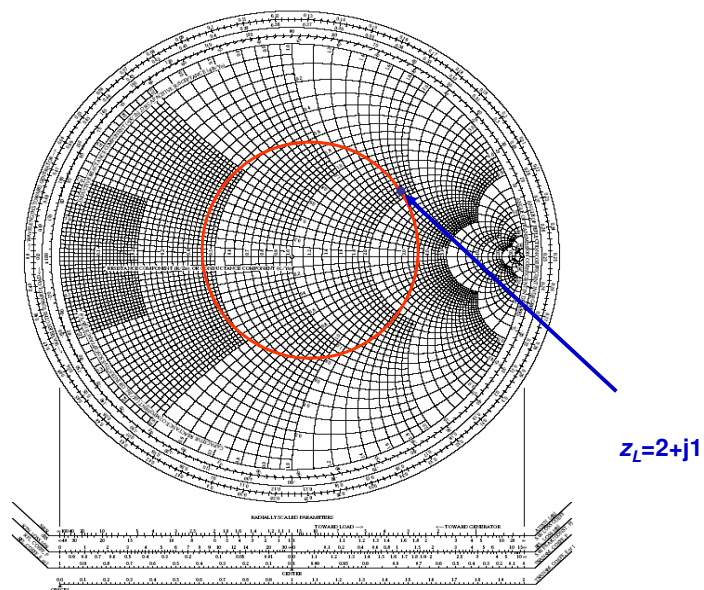
Locate  $r$  Circle of the normalized Load Impedance = Real part of  $(Z_L/Z_0)$



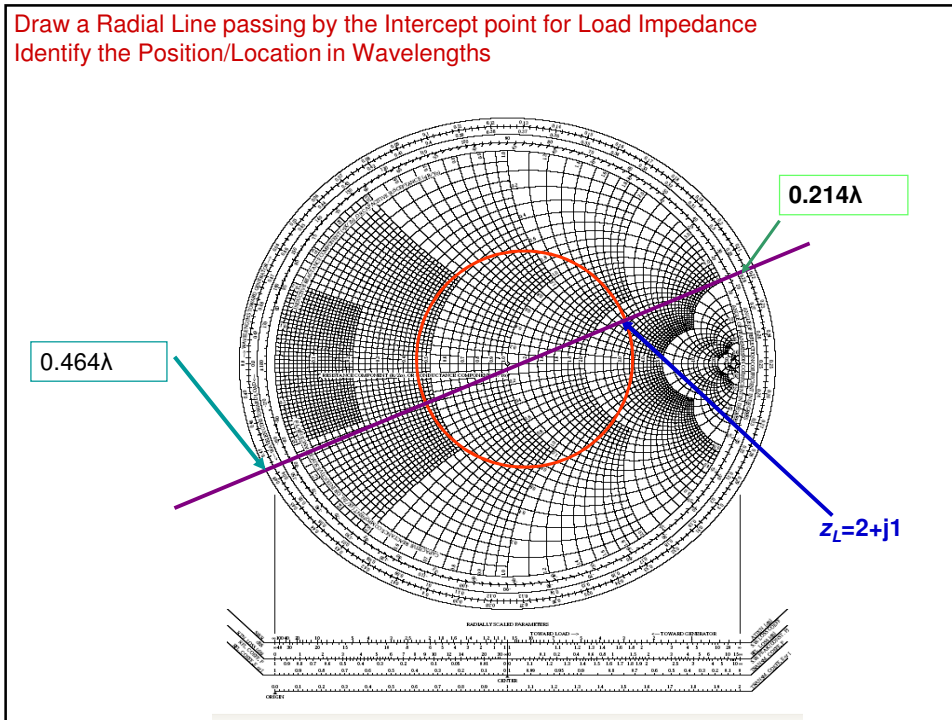
Locate the Intercept point of the r Circle and the x Circle for Load Impedance



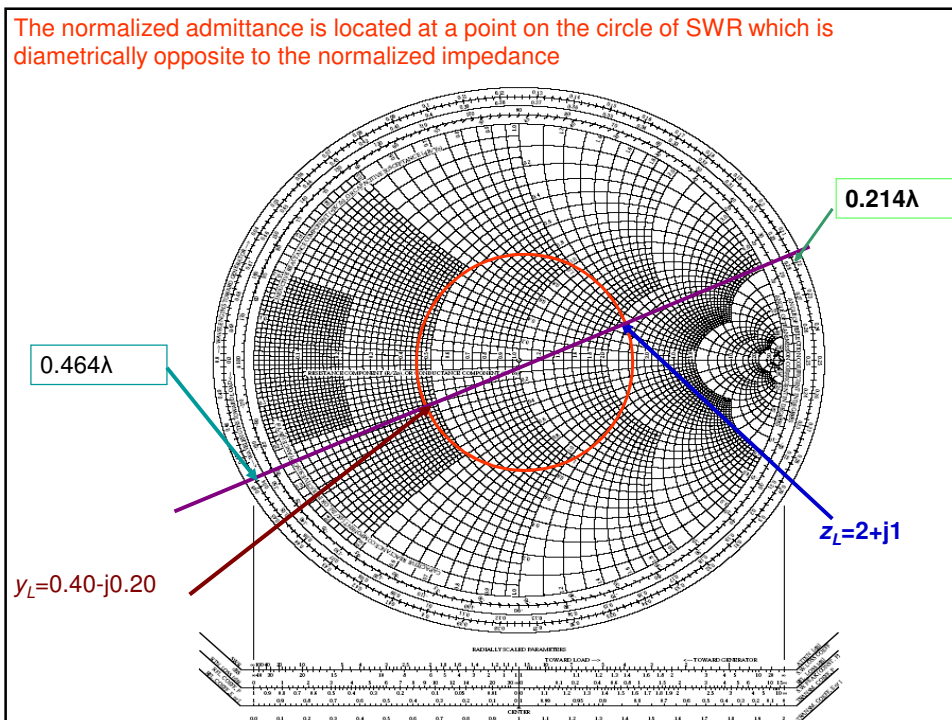
Draw the constant reflection coefficient (SWR) circle



Draw a Radial Line passing by the Intercept point for Load Impedance  
Identify the Position/Location in Wavelengths

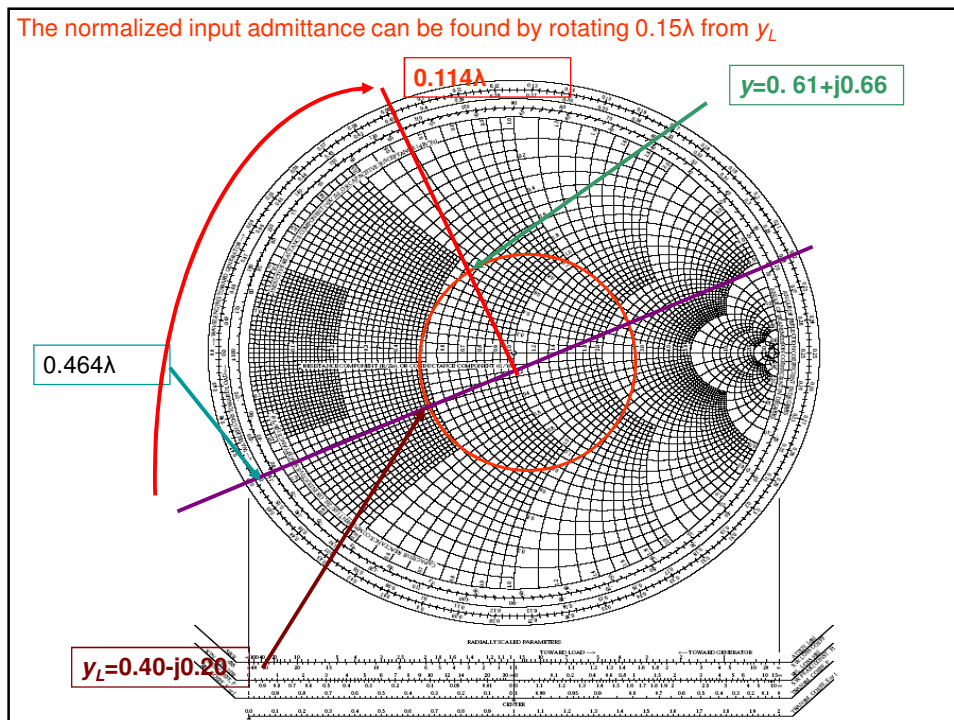


The normalized admittance is located at a point on the circle of SWR which is diametrically opposite to the normalized impedance



## The actual load admittance

- $Y_L = y_L Y_0 = y_L / Z_0 = 0.0080 - j0.0040$  (S)



## The actual input admittance

- $Y_L = yY_0 = y/Z_0 = 0.0122 - j0.00132$  (S)

## Smith Chart References

- [http://www.maxim-ic.com/appnotes.cfm/appnote\\_number/74/](http://www.maxim-ic.com/appnotes.cfm/appnote_number/74/)
- <http://www.amanogawa.com/index.html>
- [hibp.ecse.rpi.edu/~connor/education/Fields/Smith\\_Chart.ppt](http://hibp.ecse.rpi.edu/~connor/education/Fields/Smith_Chart.ppt)
- <http://tdl.ece.vt.edu/Riad/ECE4104/Handouts.htm>